

THE TERMINATED LOSSLESS T-LINE

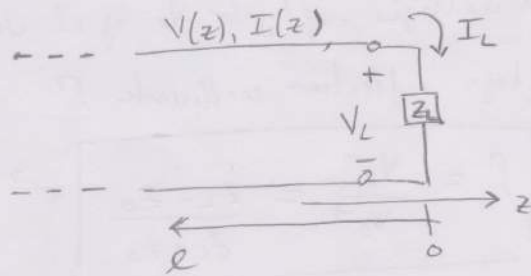


FIG 2.4) A transmission line terminated in a load impedance  $Z_L$ .

→ Assumir q' una incident de la forma  $V_0^+ e^{j\beta z}$  es generada desde una fuente a  $z < 0$ .

→ Hemos visto que la relación de voltaje a corriente para esta "traveling wave" es  $Z_0$ , que es la impedancia característica de la línea. Sin embargo cuando la línea es terminada en una carga arbitraria  $Z_L \neq Z_0$ , la relación de voltaje a corriente en la carga debe ser  $Z_L$ . Así, una onda reflejada debe poseer una amplitud q' satisfaga dicha condición.

→ El voltaje total en la línea:

$$V(z) = V_0^+ e^{-j\beta z} + V_0^- e^{+j\beta z} \quad (2.3.4a)$$

→ la corriente total

$$I(z) = \frac{V_0^+}{Z_0} e^{-j\beta z} - \frac{V_0^-}{Z_0} e^{+j\beta z} \quad (2.3.4b)$$

En la carga  $z=0$

$$Z_L = \frac{V(0)}{I(0)} = \frac{V_0^+ + V_0^-}{\frac{V_0^+ - V_0^-}{Z_0}} = \frac{V_0^+ + V_0^-}{V_0^+ - V_0^-} \cdot Z_0 = Z_L$$

resolviendo para  $V_0^-$ :

$$(V_0^+ + V_0^-) Z_0 = Z_L (V_0^+ - V_0^-)$$

$$Z_0 V_0^- + Z_L V_0^- = Z_L V_0^+ - Z_0 V_0^+ \Rightarrow V_0^- (Z_0 + Z_L) = V_0^+ (Z_L - Z_0)$$

$$V_0^- = \frac{Z_L - Z_0}{Z_L + Z_0} \cdot V_0^+$$

→ La relación entre el voltaje reflejado  $V_0^-$  y el voltaje incidente  $V_0^+$  se conoce como voltage reflection coefficient  $\Gamma$

$$\Gamma = \frac{V_0^-}{V_0^+} = \frac{Z_L - Z_0}{Z_L + Z_0} \rightarrow \boxed{V_0^- = \Gamma V_0^+} \quad (2.35)$$

→ las ondas de voltaje y corriente en la línea pueden re-emitirse.

$$V(z) = V_0^+ e^{-j\beta z} + V_0^- e^{+j\beta z}$$

$$V(z) = V_0^+ e^{-j\beta z} + \Gamma V_0^+ e^{+j\beta z}$$

$$\boxed{V(z) = V_0^+ [e^{-j\beta z} + \Gamma e^{+j\beta z}]} \quad (3.36a)$$

$$I(z) = \frac{V_0^+}{Z_0} e^{-j\beta z} - \frac{V_0^-}{Z_0} e^{+j\beta z}$$

$$= \frac{V_0^+}{Z_0} e^{-j\beta z} - \frac{\Gamma}{Z_0} V_0^+ e^{+j\beta z}$$

$$\boxed{I(z) = \frac{V_0^+}{Z_0} [e^{-j\beta z} - \Gamma e^{+j\beta z}]}$$

→ Podemos ver que el  $V$  y la  $I$  en la línea consiste de una superposición de una onda incidente y una onda reflejada.

→ a dicha onda se le conoce como: standing wave.

→ cuando  $\Gamma = 0$  → no hay onda reflejada.

→ Para obtener  $\Gamma = 0$ ,  $Z_L = Z_0$  → condición: "matched load"

Consideramos el Time-average-power along the line

$$P_{avg} = \frac{1}{2} \frac{|V_0^+|^2}{Z_0} (1 - |\Gamma|^2) \quad 2.3.7$$

Total power delivered to the load: incident power  $\frac{|V_0^+|^2}{2Z_0}$  minus the reflected Power  $(|V_0|^2 \frac{|\Gamma|^2}{2Z_0})$ .

→  $\Gamma = 0$  → max power delivered to the load.

$\Gamma = 1$  → No power delivered to the load.

→ Return Loss :

$$RL = -20 \log |\Gamma| \text{ dB}$$

$\Gamma = 0$  →  $RL = \infty$  dB (No reflected Power)

$|\Gamma| = 1$  →  $RL = 0$  dB. (all incident power is reflected)

→ Máximo voltage en la línea

$$|V_{max}| = |V_0^+| (1 + |\Gamma|)$$

→ mínimo voltage en la línea

$$|V_{min}| = |V_0^+| (1 - |\Gamma|)$$

→ Standing Wave Ratio (voltage standing wave ratio).

$$SWR = \frac{V_{max}}{V_{min}} = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

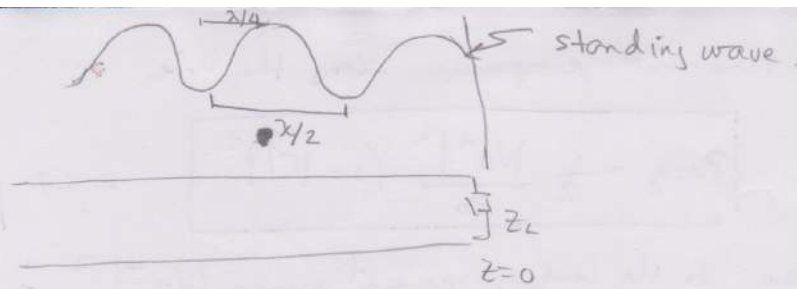
$$1 \leq SWR \leq \infty$$

$SWR = 1$  → matched load.

→ distance entre dos máximos de voltage (o mínimos)

$$l = \lambda/2$$

→ distancia entre un máximo y un mínimo:  $l = \lambda/4$



→ Reflectal coefficient en cualquier punto de la línea

$$\Gamma(l) = \frac{V_0^- e^{-j\beta l}}{V_0^+ e^{j\beta l}} = \Gamma(0) e^{-2j\beta l}$$

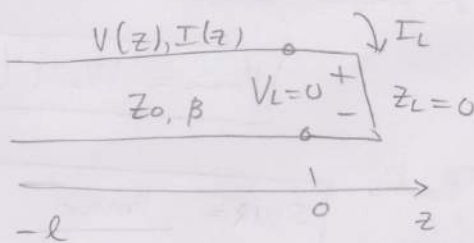
$\Gamma(0)$  = coeficiente de reflexión at  $z=0$  (load)

→ Transmission line impedance equation:

$$Z_{in} = Z_0 \frac{Z_L + j Z_0 \tan \beta l}{Z_0 + j Z_L \tan \beta l}$$

⇒ Special Cases of lossless T-line.

a)  $Z_L = 0$  short circuit



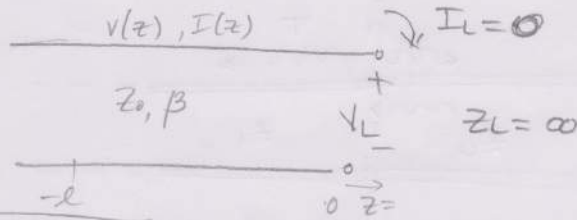
$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = -1$$

$$Z_{in} = Z_0 \frac{0 + j Z_0 \tan \beta l}{Z_0 + j(0) \tan \beta l} = \boxed{j Z_0 \tan \beta l} \quad (2.45c)$$

when  $l = 0 \rightarrow Z_{in} = 0$

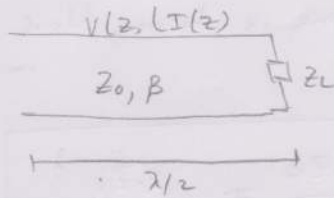
$l = \lambda/4 \rightarrow Z_{in} = \infty$  (open circuit)

b) OPEN CIRCUIT CASE



$$Z_{in} = -j Z_0 \cot \beta l$$

- LENGTH  $\lambda/2$



$$\beta l = \frac{2\pi}{\lambda} \cdot \frac{\lambda}{2} = \pi$$

$$Z_{in} = Z_0 \frac{Z_L + j Z_0 \tan \beta l}{Z_0 + j Z_L \tan \beta l} = Z_0 \frac{Z_L + j Z_0 \tan(\pi)}{Z_0 + j Z_L \tan(\pi)} = Z_L$$

$$Z_{in} = Z_L$$

- LENGTH  $\lambda/4$

$$\beta l = \frac{2\pi}{\lambda} \cdot \frac{\lambda}{4} = \pi/2$$

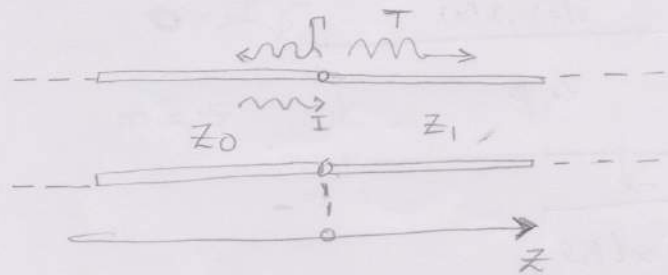
$$Z_{in} = Z_0 \frac{Z_L + j Z_0 \tan \beta l}{Z_0 + j Z_L \tan \beta l} = Z_0 \frac{Z_L + j Z_0 \tan(\pi/2)}{Z_0 + j Z_L \tan(\pi/2)}$$

$$Z_{in} = Z_0 \frac{\tan(\pi/2) \left[ \frac{Z_L}{\tan(\pi/2)} + j Z_0 \right]}{\tan(\pi/2) \left[ Z_0 \frac{Z_0}{\tan(\pi/2)} + j Z_L \right]} = Z_0 \cdot \frac{j Z_0}{j Z_L}$$

$$Z_{in} = \frac{Z_0^2}{Z_L}$$

(quarter wave transformer). // class on antennas

JOEVES 24-sept, Quiz #3.



$$\Gamma = \frac{Z_1 - Z_0}{Z_1 + Z_0}$$

Not all incident wave is reflected,  
some is transmitted

$$T = 1 + \Gamma = 1 + \frac{Z_1 - Z_0}{Z_1 + Z_0} = \frac{2Z_1}{Z_1 + Z_0}$$

Transmission  
coefficient

$$I_L = -20 \log |T| \text{ dB} \quad \text{insertion Loss}$$